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AN EFFECT OF NON-HOMOGENEOUS FIBRE PACKING ON MECHANICAL PROPERTIES OF OXIDE/NICKEL COMPOSITES

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ABSTRACT

This work generalises results obtained by the authors studying room temperature strength and creep of oxide-fibre/nickel-based-matrix composites. An effect of fibre packing in the cross-section of a composite body together with that of fibre/matrix interface strength on mechanical behaviour is analysed. It is shown that if the interface strength does not depend of fibre volume fraction, then the strongly non-homogeneous fibre packing will not yield a decrease in the creep resistance.

Keywords: metal matrix composites, oxide fibre, nickel matrix, fibre packing, creep.

INTRODUCTION

A homogeneous fibres packing in the metal-matrix composite body is normally a wanted reinforcement scheme. Optimization of a structural element will often require a special fibre packing. On the other hand, a non-homogeneous fibre distribution is often observed in specimens made to evaluate mechanical properties of the composite. Therefore, understanding an effect of non-homogeneity of the fibre packing on mechanical response of composites is an important problem of composite mechanics. The problem is complicated as various properties depend on a degree of the non-homogeneity in different ways. The composite strength at high fibre volume fractions is normally higher when the fibre packing is more homogeneous [Mileiko, 1997]. In the case of creep, the situation is not so simple, so in the present paper the authors consider mainly the creep behavior of metal-matrix composites.

RESULTS AND CONCLUSIONS

Experiments were carried out on composites with four types of oxide fibres produced by the internal crystallization method [Mileiko, 2005] and two nickel as the matrix. A dependence of creep resistance on fibre volume fraction for one composition is given in Fig. 1. This is a typical dependence: the scatter of experimental data is very large, the creep resistance reaches a maximum at some value of the fibre volume fraction. To interpret the experimental data, the following consideration should be taken into account:

1. The fibre/matrix interface strength, which is an important parameter determining creep resistance, can be constant up to a definite value of fibre volume fraction V_f and then goes down. This effect was found in experiments with specimens with sufficiently homogeneous fibre packing [Mileiko et al., 2002].
2. This effect can influence local areas of the specimen cross-section with high fibre concentration forming fibre clusters with low interface strength.
3. In power function $\dot{\epsilon} = \eta (\sigma / \sigma_n)^n$ describing the dependence of creep rate $\dot{\epsilon}$ on stress, constants σ_n and n depend on fibre volume fraction [Mileiko, 2002].

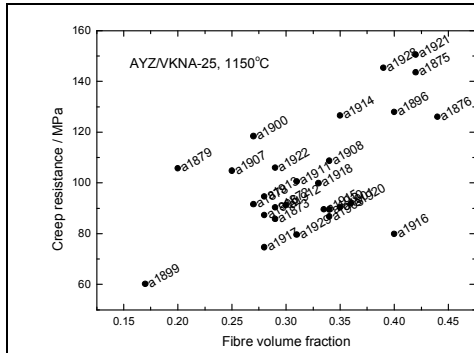


Fig. 1 - Creep resistance of the Al_2O_3 - $\text{Y}_3\text{Al}_5\text{O}_{12}$ - ZrO_2 -eutectic-fibre/VKNA25-matrix composites versus fibre volume fraction.

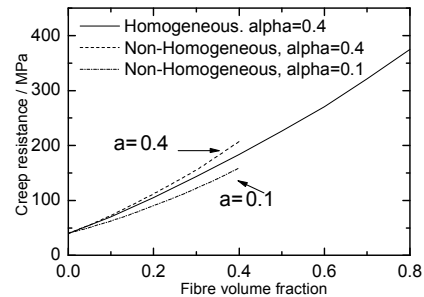


Fig. 2 - Dependencies of creep resistance of composite models with homogeneous and non-homogeneous fibre packing on average fibre volume fraction for relatively strong interface ($\alpha = 0.4$). The same dependence for a model with weak interface ($\alpha = 0.1$) and non-homogeneous fibre packing.

These experimental observations allow calculating creep resistance of composites with non-homogeneous fibre packing. In the full-text paper a simple model example is considered to compare creep resistance of two composite specimens. The first one is characterized by homogeneous fibre distribution, $V_f = V_f^0$. The fibre distribution in the second one is highly non-homogeneous. A half of the cross-section does not have fibres at all, the other half has a homogeneous fibre distribution, $V_f = 2V_f^0$. The calculation was performed for two values of the non-dimensional fibre/matrix interface strength, $\alpha_1 = 0.1$ and $\alpha_2 = 0.4$.

The calculated dependencies are plotted in Fig. 2. Comparing the data obtained with the experimental data (Fig. 1) yields the following main conclusion:

If the fibre/matrix interface strength does not depend of fibre volume fraction, then the strongly non-homogeneous fibre packing will not yield a decrease in the creep resistance. The assumption mentioned does not applicable to the composites, of which creep behavior is like that shown in Fig 1.

ACKNOWLEDGMENTS

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